Handbooks for the design, installation and verification of seismic protection for fire sprinkler systems

nVent CADDY We Make Seismic Simple nvent

Hari Kumar / Olivier Braquet Thursday 9 May 2024

Seismic damage to/from a fire sprinkler system without seismic sway bracing





Seismic damage to a piping system





No clearance



Seismic damage to not anchored equipment





Tip over



Seismic damage to not anchored equipment



Glissement



A changing world



Fire protection systems and seismic protection

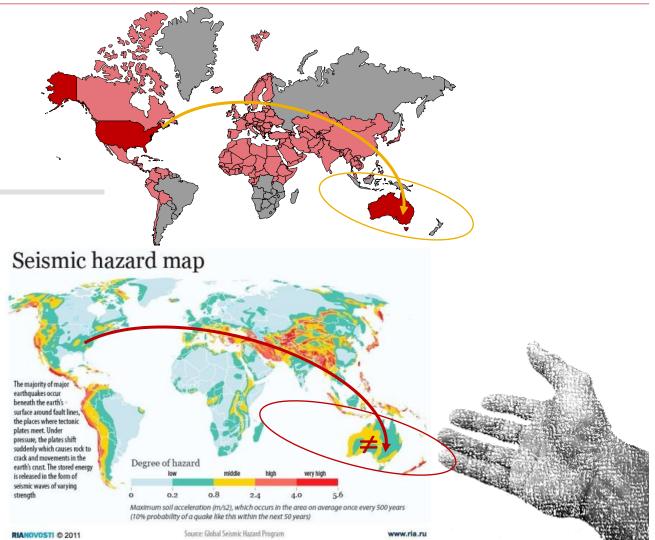
Fire Protection Fire Sprinkler Standards (from USA) NFPA 13 FM Global

Seismic protection Seismic standard AS 1170.4 Performance based

Operability of strategic infrastructures Immediately after and earthquake

Operability of life-safety systems (fire protection systems)

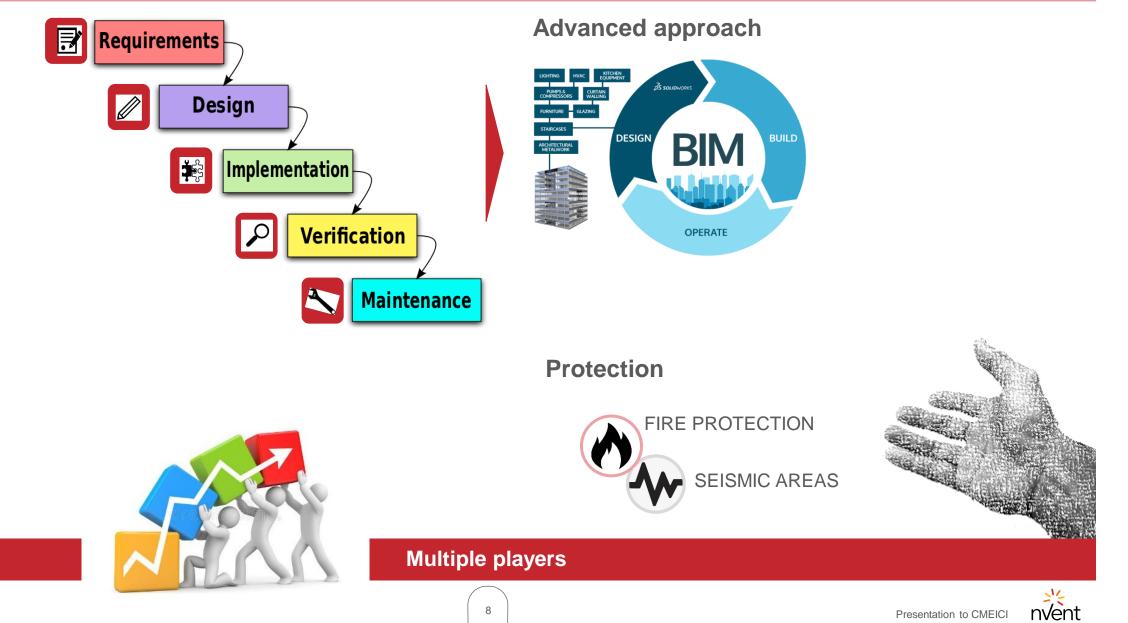
Seismic protection of life-safety systems (seismic protection of sprinkler systems)



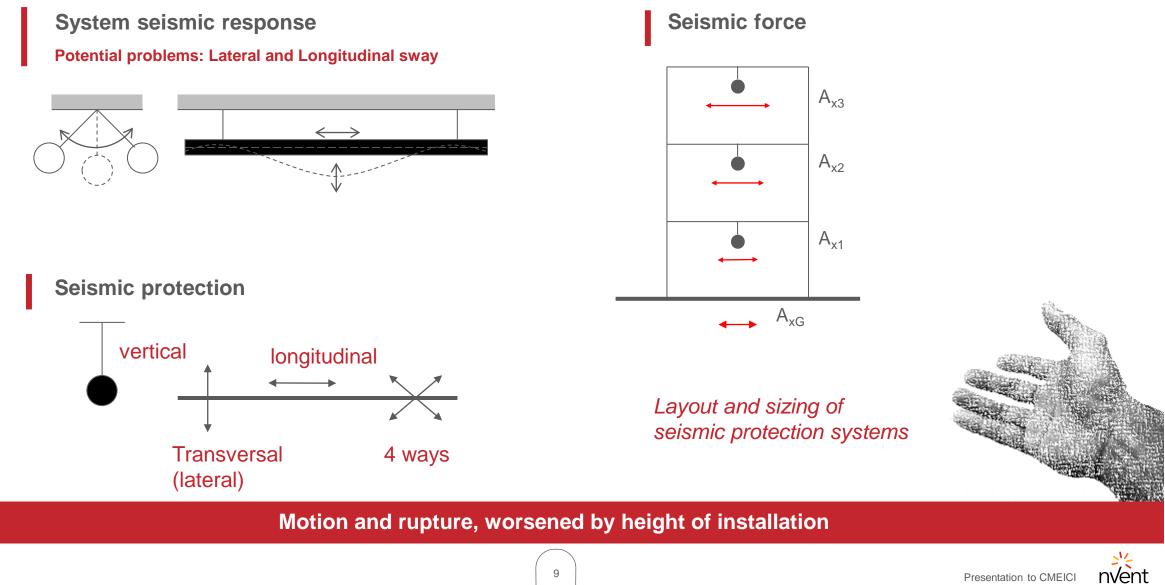
"Extension" of the use of fire sprinkler standards but different seismic standards contexts



The system realization process

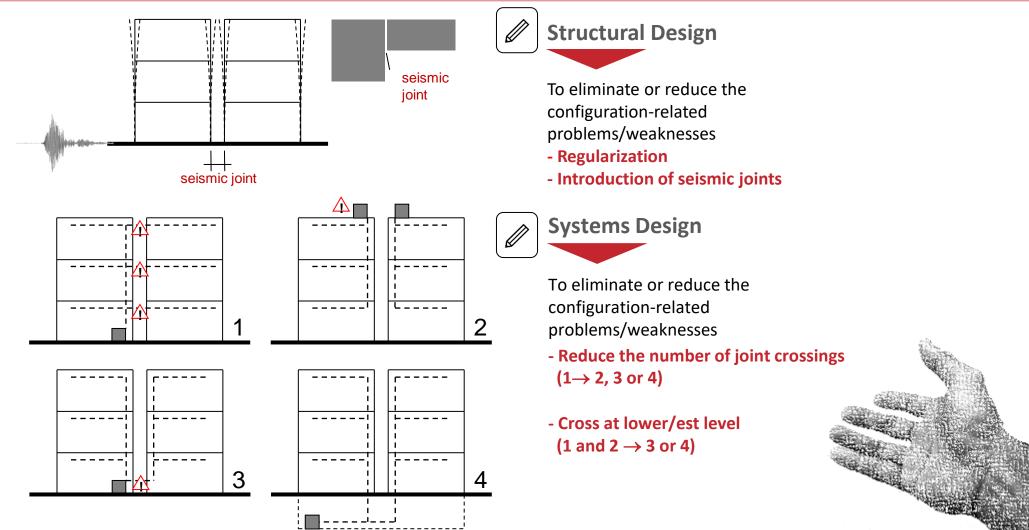


Piping systems seismic challenges



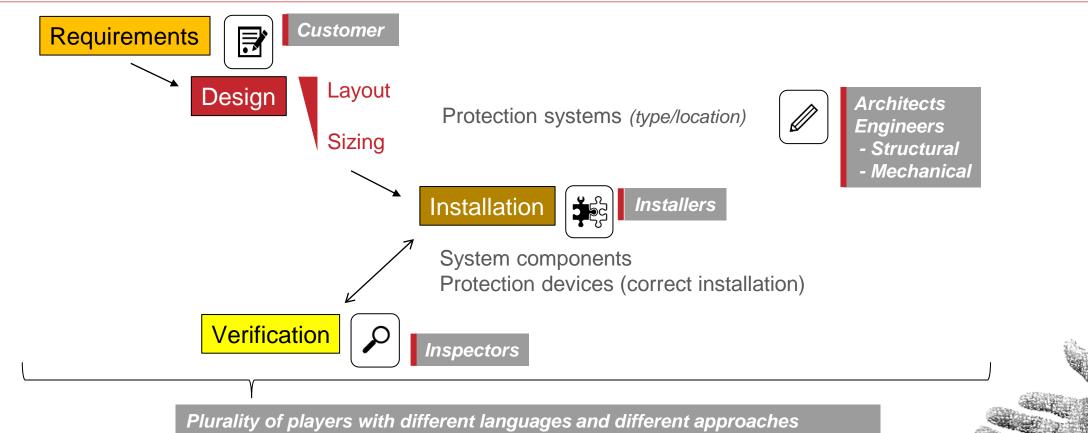
Presentation to CMEICI

Integrated seismic design



Smart seismic structural design and seismic system design choices reduce the seismic risk

Many players



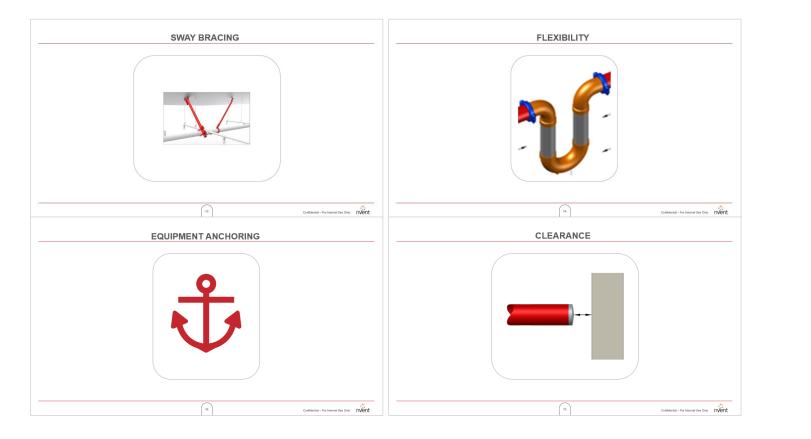


Interface support and common reference tools could play an important role





The 4 aspects of an effective seismic protection

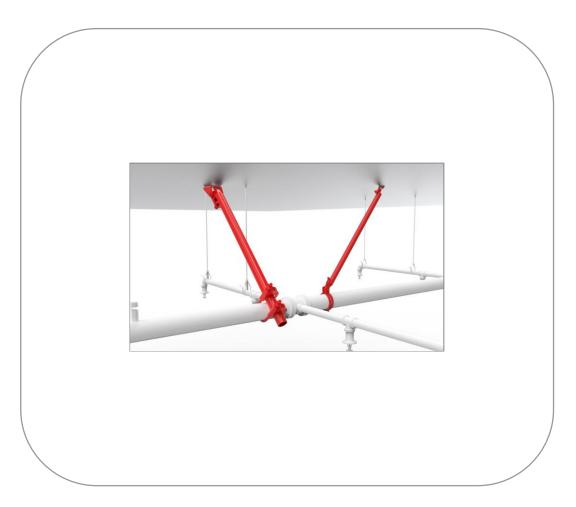






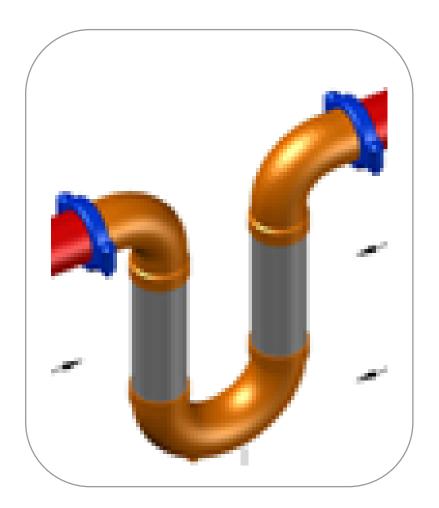
Presentation to CMEICI

SWAY BRACING

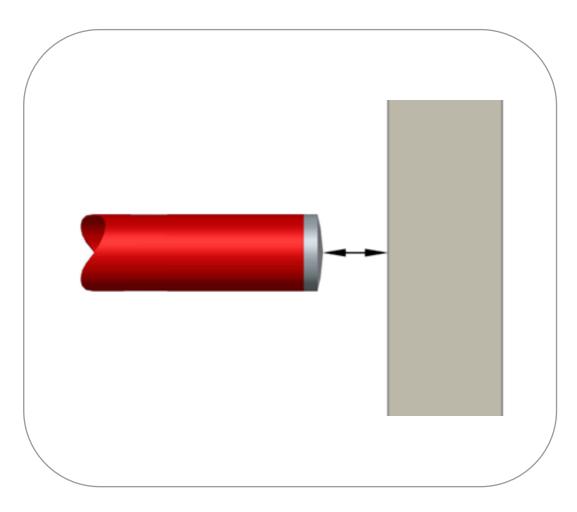




FLEXIBILITY



CLEARANCE



EQUIPMENT ANCHORING



The 4 pillars of a sound seismic protection











The 4 pillars of a sound seismic protection





















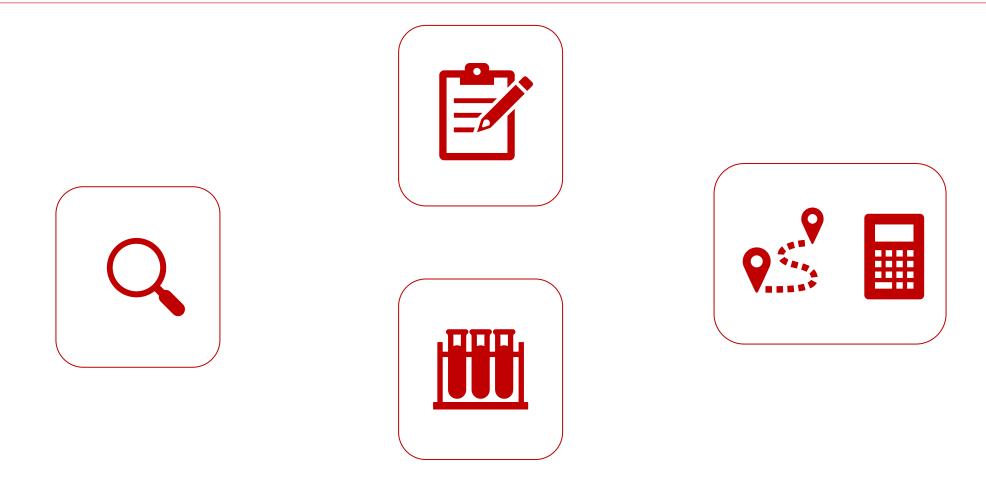








ງ ເ The 4 pillars of a sound seismic protection



1. Agreed upon requirements – 2. Load path calculation –

3. Use products tested for seismic protection application – 4. Independent verification of the installation



Manifolded Risers







Manifolded Risers



Start from «Sway bracing» section 2.2.1.1 Sway Bracing Locations for Steel Piping

Guidance in this section applies to steel pipe. See 2.2.1.9 for other pipe materials.

2.2.1.1.1 At a minimum, locate and space sway bracing for sprinkler system (ceiling and in-rack) and hose system steel piping per this section. Braces and their attachments must also be sized to resist design forces per 2.2.1.2 and configured per 2.2.1.3. Provide additional sway braces when necessary to reduce the tributary load so the brace capacity is not exceeded or so sway bracing locations will coincide with adequate structural members to which the sway braces will be attached. Also see further commentary in Section 3.1.2.

2.2.1.1.2 Provide adequately sized and configured bracing on sprinkler system risers, whether they are single or manifolded type and regardless of size, in accordance with the following guidelines. Also see further commentary in Section 3.1.3.

2.2.1.1.2.1 Provide a four-way sway brace within 2 ft (0.6 m) of the top of each riser. When possible, avoid the use of a single manifolded sway bracing assembly at the top of multiple adjacent risers. If used, limit the manifolded arrangement to two risers.

2.2.1.1.2.2 In multistory buildings, provide a four-way brace on the riser within 2 ft (0.6 m) of each building floor level. A four-way brace can be considered to exist when the riser passes through a structural floor and clearances do not allow more than ½ in. (13 mm) movement in any horizontal direction (note: this arrangement will require additional flexible couplings on the riser; see 2.2.1.4.3.3).

2.2.1.1.2.3 Provide additional intermediate four-way sway bracing on risers at an interval not to exceed 40 ft (12.2 m). Where flexible couplings are used, arrange this intermediate four-way sway bracing so a brace is provided within 2 ft (0.6 m) of every other flexible coupling (adding four-way braces if necessary). For risers in multistory buildings or towers that have attached feed or cross mains not located at floor levels, add four-way braces if necessary such that a brace is provided within 2 ft (0.6 m) of these mains.

2.2.1.1.2.4 For risers fed from horizontal manifold piping, provide a two-way lateral sway brace within 2 ft (0.6 m) of the end of any horizontal manifold piping longer than 6 ft (1.8 m), or when any flexible couplings are used on either the horizontal manifold piping or on the riser stub between the floor and the connection to the horizontal manifold piping. See Fig. 2.2.1.1.2.





Manifolded Risers



Start from «Sway bracing» section

> Continue with the "Flexibility" section

to the horizont

Guidance in this section applies to steel pipe. See 2.2.1.9 for other pipe materials.

2.2.1.1 Sway Bracing Locations for Steel Piping

2.2.1.1.1 At a minimum, locate and space sway bracing for sprinkler system (ceiling and in-rack) and hose system steel piping per this section. Braces and their attachments must also be sized to resist design forces per 2.2.1.2 and configured per 2.2.1.3. Provide additional sway braces when necessary to reduce the tributary load so the brace capacity is not exceeded or so sway bracing locations will coincide with adequate structural members to which the sway braces will be attached. Also see further commentary in Section 3.1.2.

2.2.1.1.2 Provide adequately sized and configured bracing on sprinkler system risers, whether they are single or manifolded type and regardless of size in accordance with the following guidelines. Also see further commentary in 2.2.1.4 Flexibility Needed to Allow Differential Movement

2.2.1.1.2.1 Prov 2.2.1.4.1 Provide adequate flexibility between portions of properly braced, welded and non-welded sprinkler the use of a sin systems, regardless of pipe size, that are expected to move differentially with respect to each other using the manifolded the following guidelines and techniques.

2.2.1.1.2.2 In m Guidance in this section applies to steel pipe. See 2.2.1.9 for other pipe materials. floor level. A fou

clearances do n 2.2.1.4.2 If more flexible couplings are installed than recommended in this section, provide additional lateral will require add sway bracing to prevent excessive movement of piping per 2.2.1.1.2.3, 2.2.1.1.4.3 and 2.2.1.1.5.1.E. 221123 Prov

ft (12.2 m). Whe 2.2.1.4.3 Provide flexibility for sprinkler risers per the following recommendations.

provided within 2.2.1.4.3.1 Provide a flexible coupling within 2 ft (0.6 m) of the top and bottom of each individual riser that in multistory bu is connected directly to underground piping (see Fig. 3.1.3 in the Section 3.1.3 commentary for details). This four-way braces applies to risers located outside and inside buildings. Where welded piping systems exist from the riser 2.2.1.1.2.4 For through the cross mains, the flexible coupling at the top of the riser may be omitted (0.6 m) of the e

are used on eit 2.2.1.4.3.2 When multiple risers are supplied by a single manifold connection to an underground main, provide each riser with a flexible coupling within 2 ft (0.6 m) of the top, and a flexible coupling within 2 ft (0.6 m) of the bottom where connected to the manifold, Locate the horizontal manifold piping 3 ft (0.9 m) or less above floor level and brace manifold piping when needed (see 2.2.1.1.2.4). Connect the horizontal manifold to the main riser and the main riser to the riser stub at floor level with flanged or other rigid connections (see Fig. 2.2.1.1.2). Where welded piping systems exist from the riser through the cross mains, the flexible coupling at the top of the riser may be omitted.

> 2.2.1.4.3.3 For multistory building risers, additional flexible coupling(s) are needed at each floor level. When the pipe doesn't penetrate a floor slab, steel plate, etc. (e.g., is in an open tower), or when it does penetrate one of these elements and clearances meet the recommendations of 2.2.1.5.1, locate the flexible coupling within 1 ft (0.3 m) of the floor (either above or below the floor; see Fig. 2.2.1.4.3). Where clearances per 2.2.1.5.1 are not provided, install flexible couplings within 1 ft (0.3 m) both above and below the floor. (Exception: the flexible coupling below the floor should be located below any main supplying that floor.)

2.2.1.4.3.4 Flexible couplings are not needed on riser piping beneath floors that rest directly on the ground; however, a flexible coupling is needed above the ground floor as recommended in 2.2.1.4.3.1 and 2.2.1.4.3.2.

2.2.1.4.3.5 Provide a flexible coupling within 2 ft (0.6 m) above or below any intermediate points of bracing for risers. Where welded piping systems exist from the riser through the cross mains, these flexible couplings may be omitted.





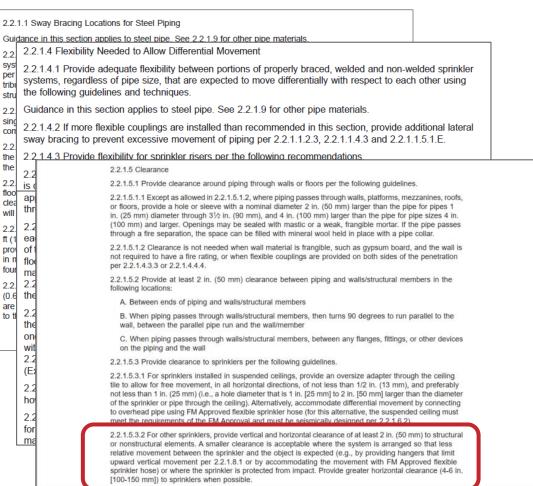
Manifolded Risers



Start from sway bracing section

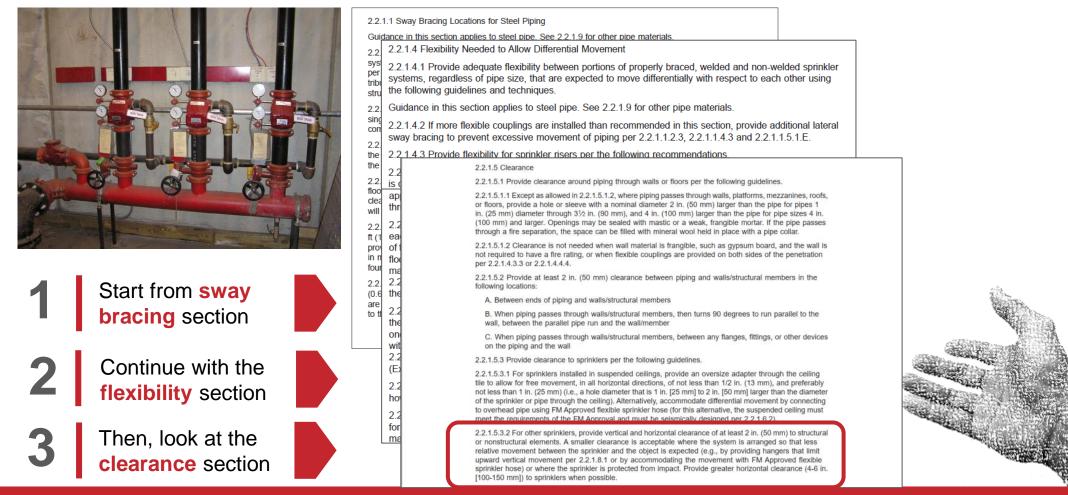
Continue with the flexibility section

Then, look at the clearance section





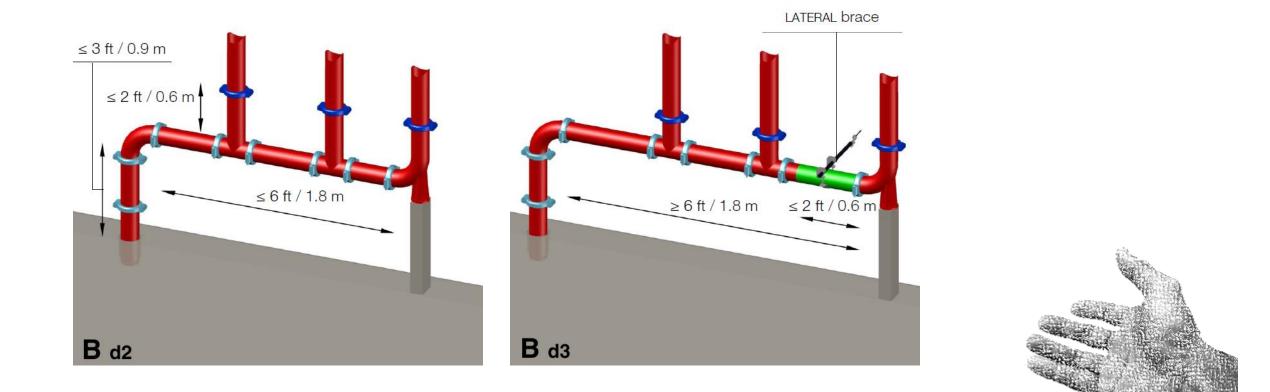
Manifolded Risers



How to explain to a non-expert? How do the multiple players get on the same page?



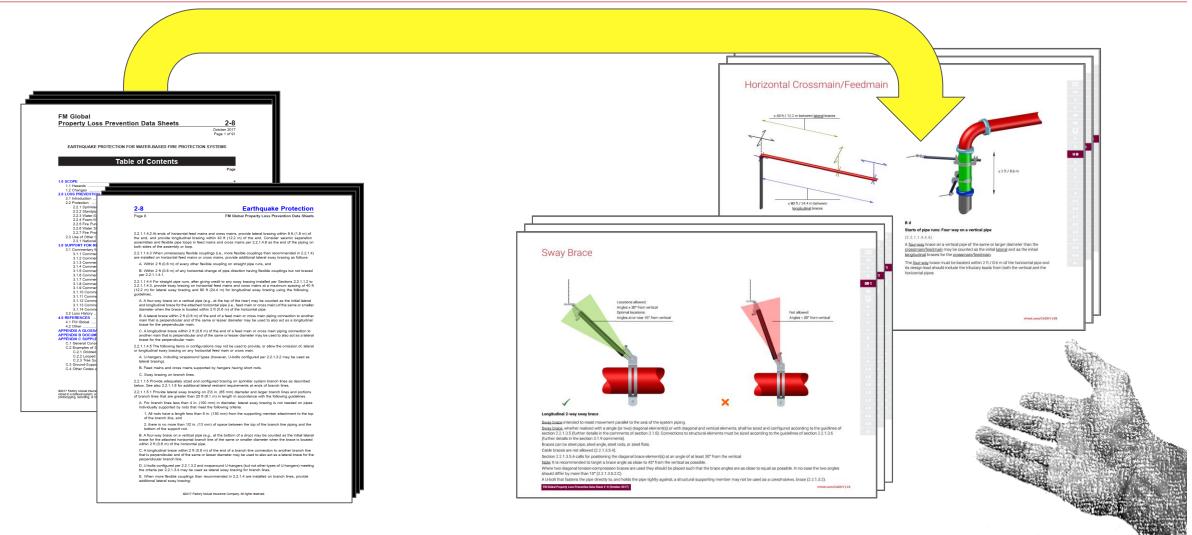
Manifolded Risers



Illustrations is the answer



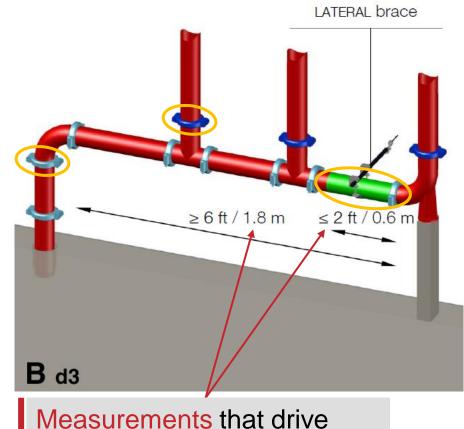
"Translation" into a visual language



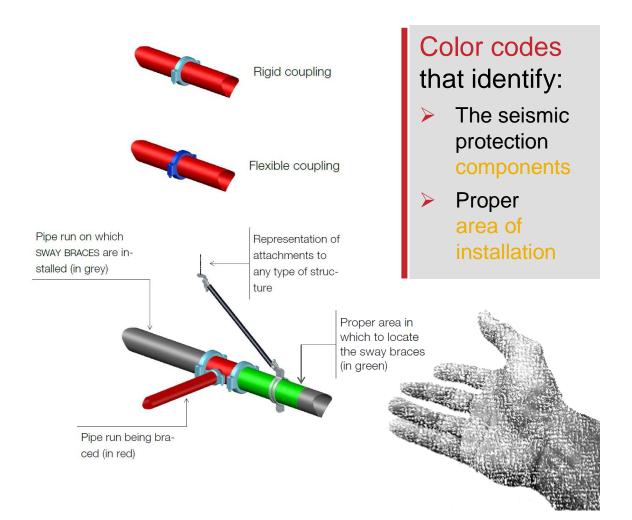
A picture is worth 1000 words



Color coding

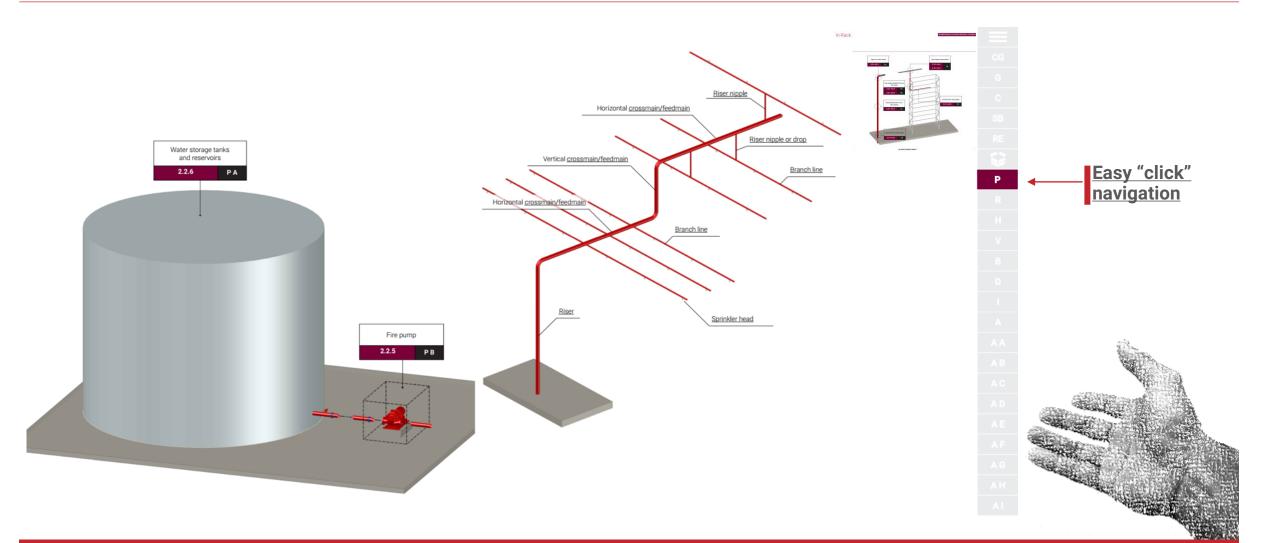


Measurements that drive requirements for seismic protection components





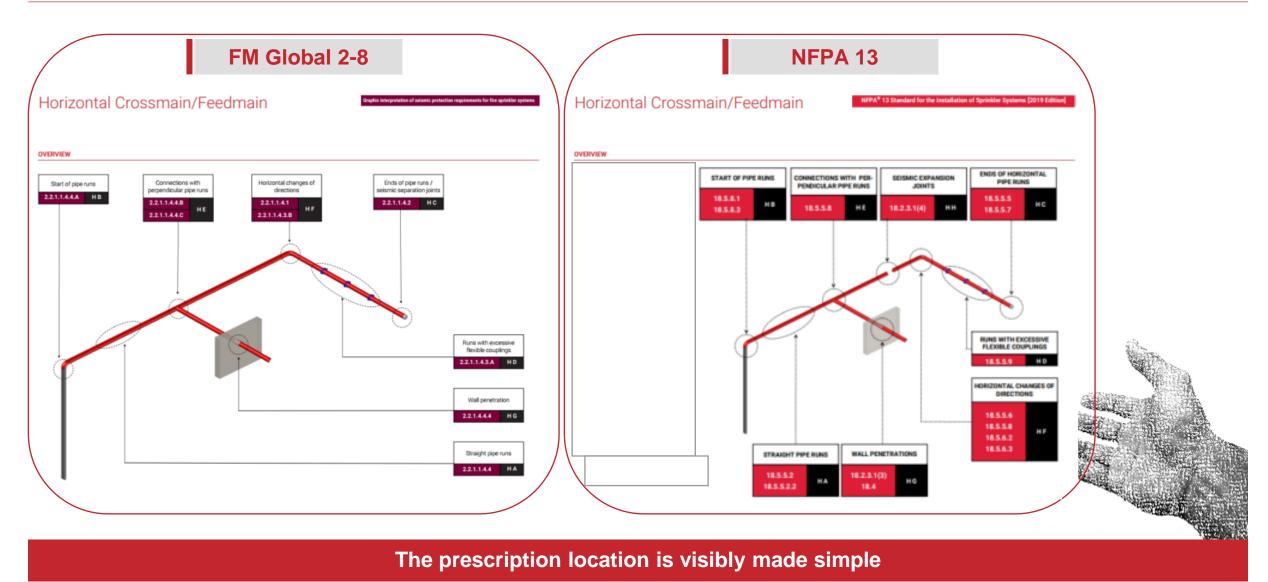
Logically ordered



Easy to Navigate



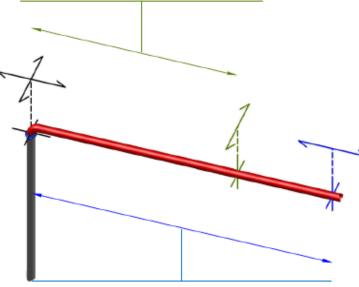
Layout of seismic protection components



Presentation to CMEICI

Illustrations for the layout & illustrations for the installation

≤ 40 ft / 12.2 m between LATERAL braces

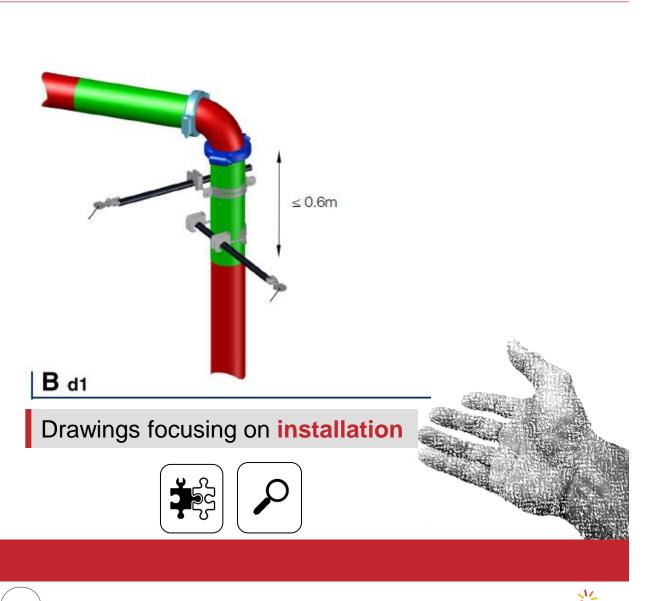


≤ 80 ft / 24.4 m between LONGITUDINAL braces

В

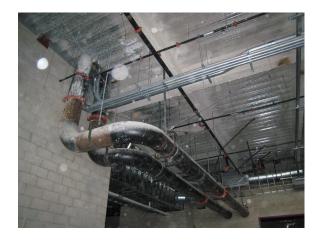
Drawings focusing on layout





nvent

Jobsite complex situations











Not detailed in standards



Complex applications

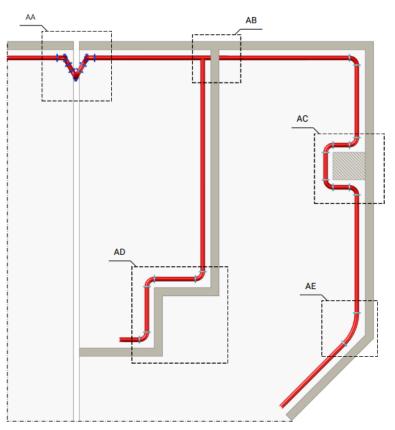
Section view

AF) Riser with offsets, vertical changes of directions

AG) Obstacles avoidance-Beams

AH) Floor penetrations

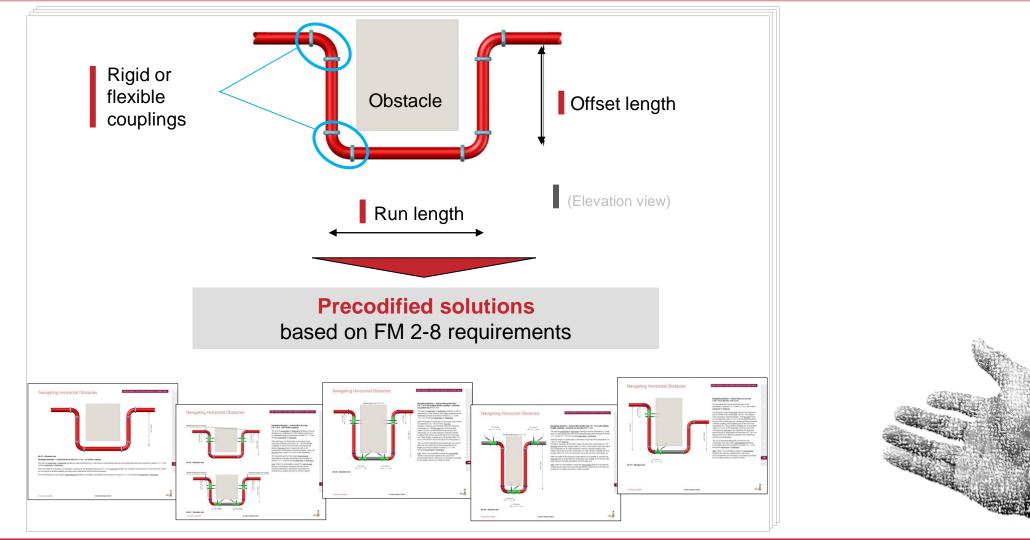
AI) Sloped ceilings



Plan view
AA) Crossing of seismic expansion joints
AB) Wall penetrations
AC) Obstacles avoidance
AD) Horizontal changes of directions: 90°
AE) Horizontal changes of directions: not at 90°

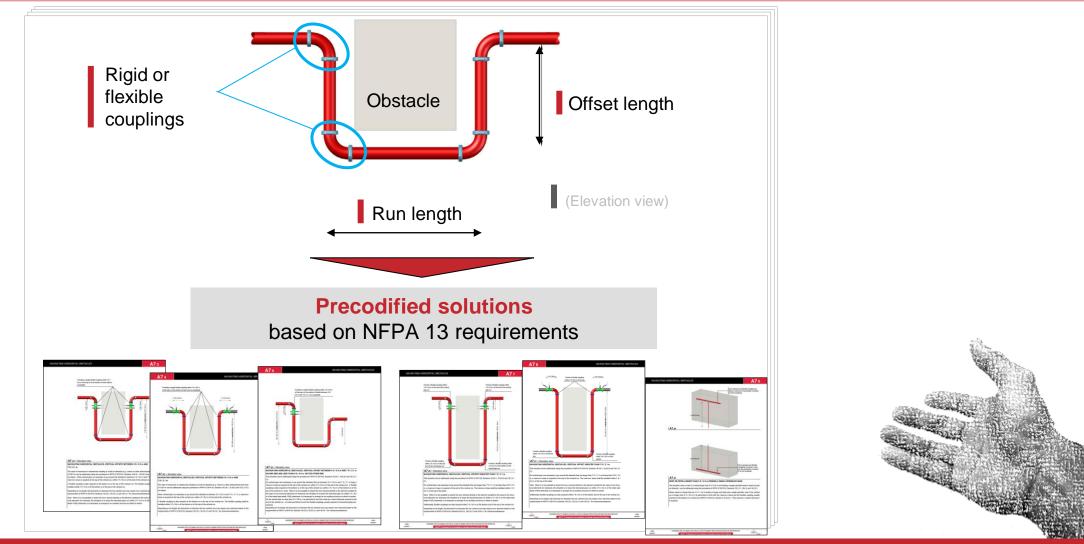


Complex applications



Compliant solutions made simple

Complex applications

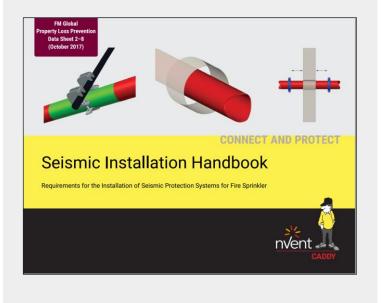


Compliant solutions made simple

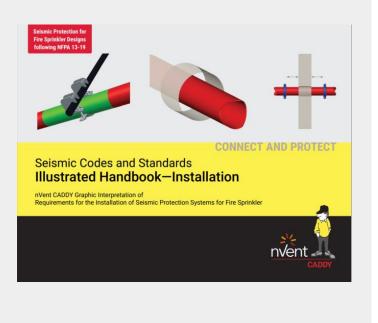


Handbooks for different standards

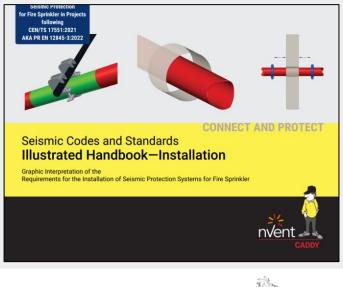
For projects insured by FM Global



For projects per NFPA 13



For projects per EN 12845





For recognized standards around the world



3-Contents per standard

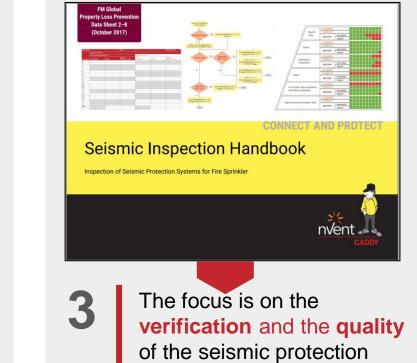
nVent CADDY Seismic Installation Handbooks





The focus is on the load path calculation and the sizing of

nVent CADDY Seismic Inspection Handbooks



3 books per standard / multiple standard per content



Installation instructions



Clearance, sway bracing, restraints



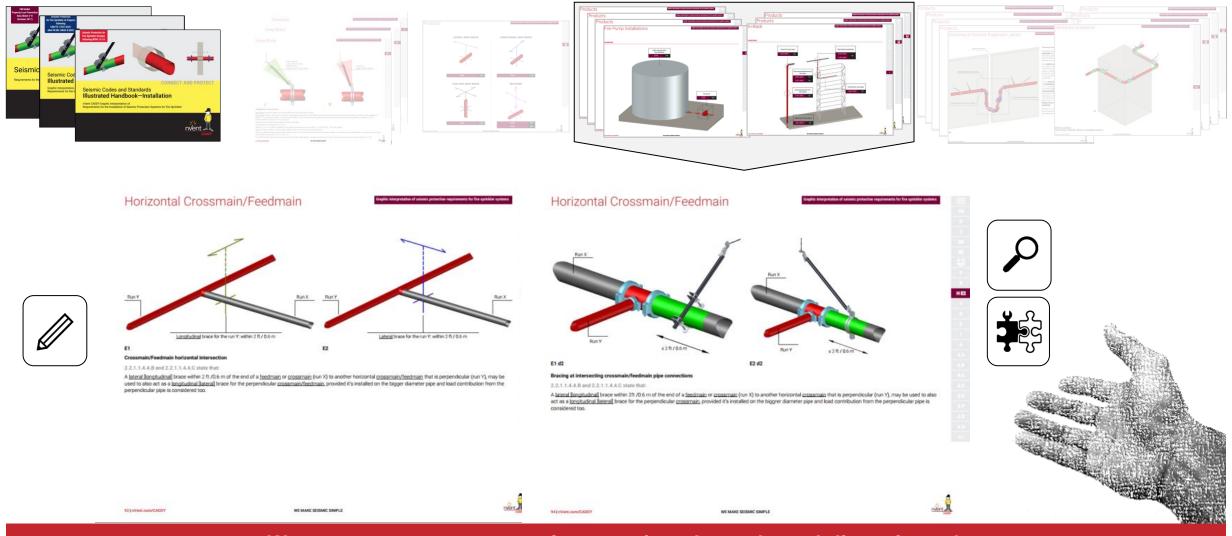
Products and assemblies



For sway bracing and for restraining



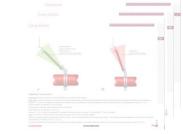
Requirements per major portions of the sprinkler system

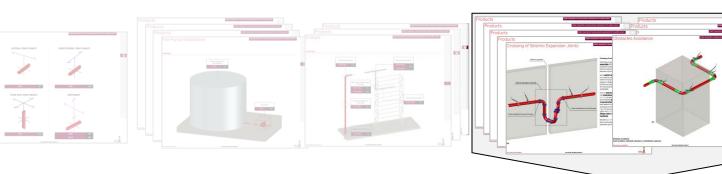




"Turn-key" compliant solutions to complex applications

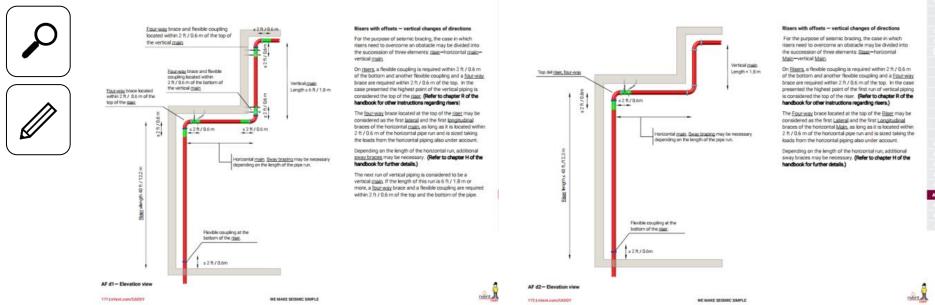






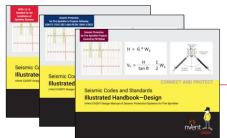
Risers with Offsets

Risers with Offsets



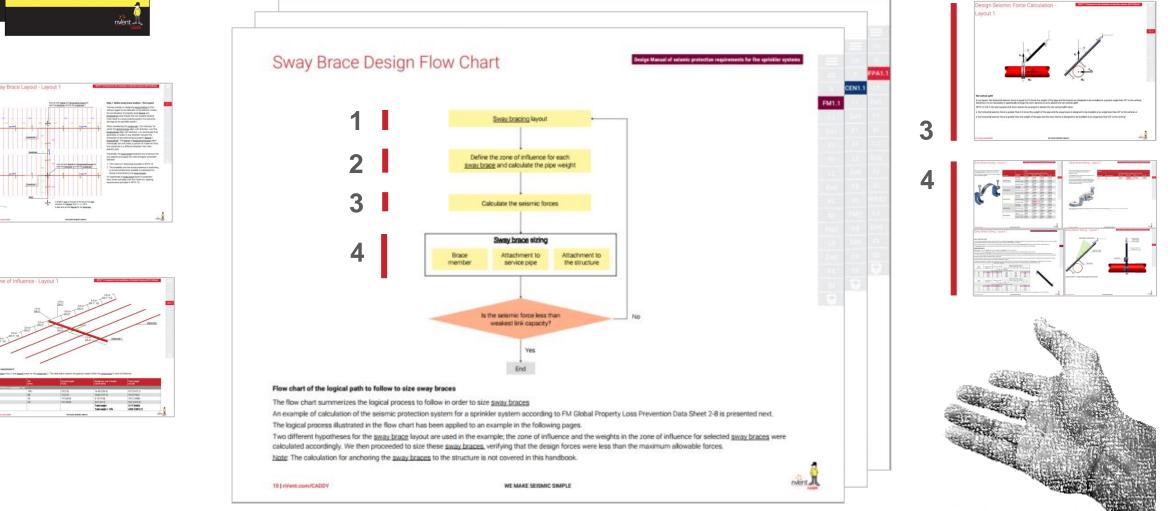
Obstacles, changes of direction, seismic expansion joints, floor & wall penetration, slopped ceilings...





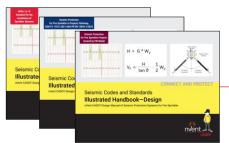
2

Sway bracing design



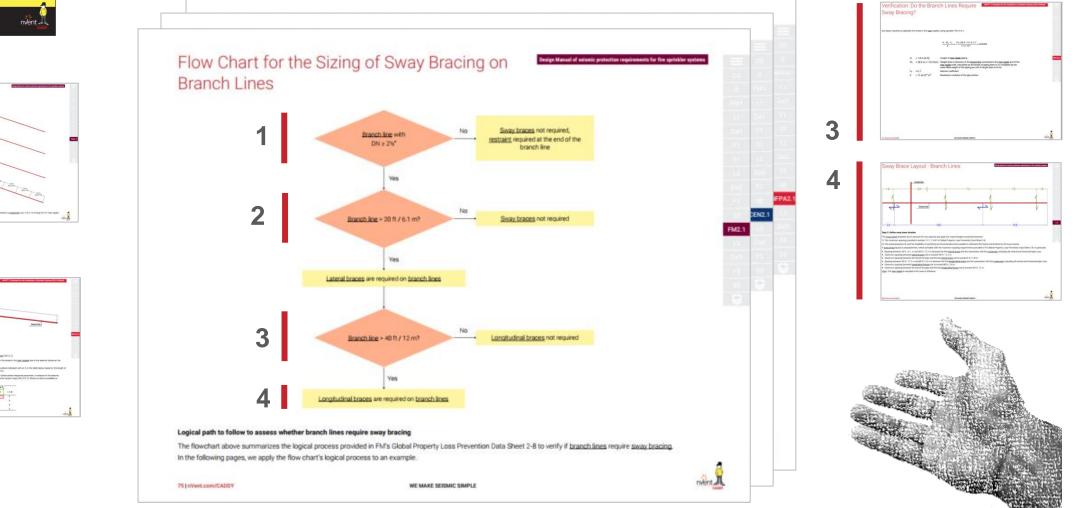
Layout – zone of influence – design seismic force calculation – assembly products selection



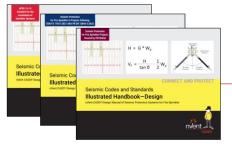


2

Verification: do the branch lines require sway bracing?



Flow chart, example



Visualization

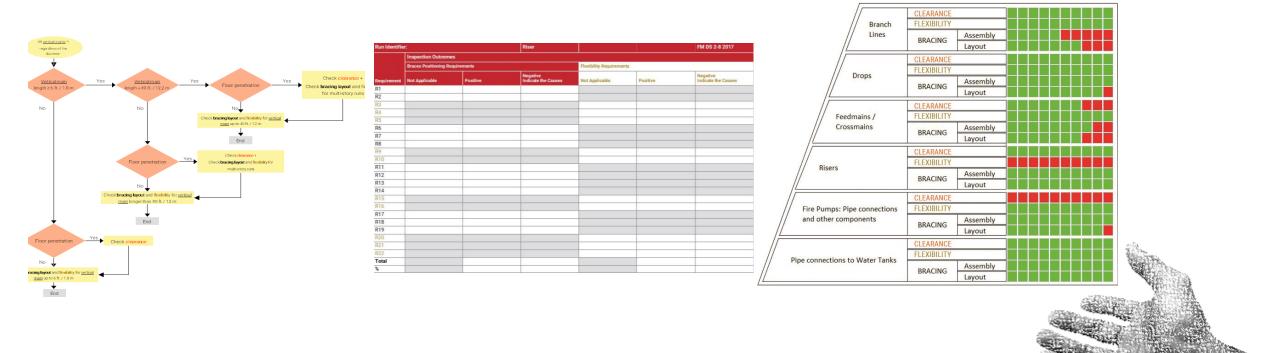


Four-way, lateral (transverse), longitudinal sway braces, and restraints





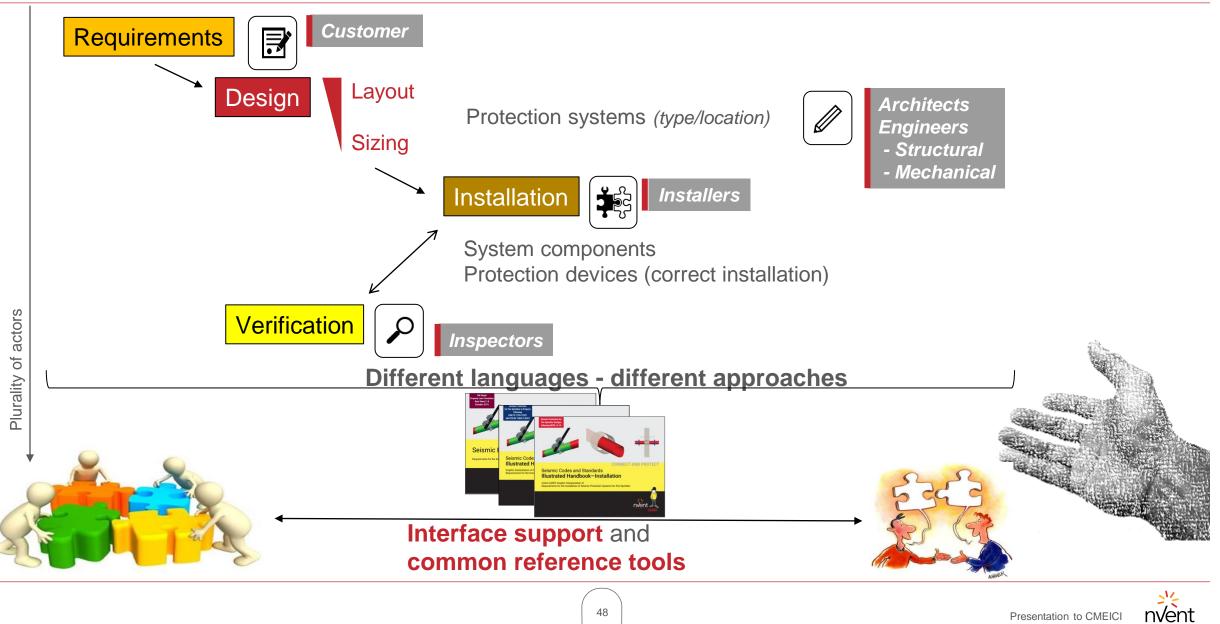
Verification



Flow charts, collection charts, proprietary pyramid to evaluate compliance and quality



Final considerations



Handbook: a **facilitator** for the **dissemination** of a



culture of Integrated / Contextualized Protection

Requests for Handbooks can be submitted at https://go.nvent.com/Seismic-Handbook-FM2017.html

Facilitator of integrated and contextualized fire and seismic protection



Thank you for your attention

Requests for Handbooks can be submitted at <u>https://go.nvent.com/Seismic-Handbook-FM2017.html</u>



Professor Stefano Grimaz

- Chairholder of the UNESCO Chair on Intersectoral Safety for Disaster Risk Reduction and Resilience
- Director of Safety and Protection Intersectoral Laboratory (SPRINT_Lab) at Polytechnic Department of Engineering and Architecture of the University of Udine
- Professor of Engineering Seismology and Safety and Civil Protection and Engineering and Safety Management and Resilience
- Scientific Consultant of national and international institutions and organizations
- From Udine, Italy





For the installation of Seismic Protection Systems for Fire Sprinkler in Projects Insured by FM Global

August 2023







- Founded in 1978
- Founded as part of the reconstruction plan from the Friuli earthquake in 1976

The authors all have a personal history with the consequences of earthquakes

